### DAV PUBLIC SCHOOLS, ODISHA ZONE

**HALF YEARLY EXAMINATION(2023-24)** 

**SUBJECT: PHYSICS (SET-2)** 

CLASS: XII

Time: 3 hours

Max. Mark:70

	BLUE PRINT OF QUESTION PAPER							
S.L NO	Name of the Chapters	Marks Allotted	MCQ& AR	SA-I 2	SA-II 3	CB 4	LA 5	Total Marks
•		in syllabus	1mark	marks	marks	mark s	mark s	
1	Electric charges & Fields	5,114.5 (15)	2 [2MCQ]	1	1		1	12
2	Electrostatic potential & Capacitance	31	1 [1MCQ]	1	1	1		10
3	Current electricity		4 (3MCQ+ 1-AR)	1	1			9
4	Moving charges & Magnetism	34	2 (1MCQ+ 1-AR)	1	1		1	12
5	Magnetism & Matter		1 [1MCQ]		1			04
6	Electromagnetic induction		2 [2MCQ]	1		1		08
7	Alternating current		2 (1MCQ+ 1-AR)		1		1	10
8	Electromagnetic Waves	05	2 (1MCQ+ 1-AR)		1			05
Tota	1	70	1× 16 = 16	2 × 5 = 10	$3 \times 7 = 21$	4 × 2 = 8	5 × 3 = 15	70

ANNEXURE-B

# DAV PUBLIC SCHOOLS, ODISHA ZONE HALF YEARLY EXAMINATION(2023-24)

**SUBJECT: PHYSICS (SET-2)** 

CLASS :XII Max.Marks:70

Time: 3 hours

#### **QUESTION WISE ANALYSIS**

QUESTION WISE ANALYSIS						
Q.NO.	CHAPTERS	FORMS OF QUESTION	MARKS ALLOT TED	(R),(U),(A), (Analyzing, Evaluating, Creating)		
1	Alternating Current	MCQ	1	A		
2	Electric charges & Fields	MCQ	1	A		
3	Electrostatic potential &	MCQ	1	U		
	Capacitance	3.600				
4	Current electricity	MCQ	1	A		
5	Current electricity	MCQ	1	U		
6	Current electricity	MCQ	1	R		
7	Moving charges & Magnetism	MCQ	1	U		
8	Magnetism & Matter	MCQ	1	R		
9	Electromagnetic Induction	MCQ	1	A		
10	Electromagnetic Induction	MCQ	1	A		
11	Electric charges & Fields	MCQ	1	U		
12	Electromagnetic Waves	MCQ	1	R		
13	Electromagnetic Waves	MCQ (AR)	1	Analyse		
14	Current electricity	MCQ(AR)	1	Analyse		
15	Moving charges & Magnetism	MCQ (AR)	1	Analyse		
16	Alternating Current	MCQ(AR)	1	Analyse		
17	Electric charges & Fields	SA-I	2	R+ U		
18	Electrostatic potential &	SA-I	2	U		
	Capacitance					
19	Current electricity	SA-I	2	A		
20	Moving charges & Magnetism	SA-I	2	R + U		
21	Electromagnetic Induction	SA-I	2	Analyse		
22	Electric charges & Fields	SA-II	3	U		
23	Electrostatic potential &	SA-II	3	A		
24	Capacitance Current electricity	SA-II	3	U		
25	Moving charges & Magnetism	SA-II	3	C		
26	Magnetism & Matter	SA-II	3	U		
27	Alternating current	SA-II	3	E		
28	Electromagnetic waves	SA-II	3	A		
20	Licenomagnetic waves	DV-II		Λ		

29	Electrostatic potential &	СВ	4	A + E + C
	Capacitance			
30	Electromagnetic Induction	CB	4	A + E + C
31	Alternating current	LA	5	A+ U +C
32	Electric charges & Fields	LA	5	R+U+A
33	Moving charges & Magnetism	LA	5	A+E+C
TOTAL			70	

Remembering &Understanding:	27Marks	38%
Application:	22Marks	32%
Analyzing, Evaluating & Creating	21Marks	30%
TOTAL	70Marks	100%

ANNEXURE-C

#### DAV PUBLIC SCHOOLS, ODISHA ZONE HALF YEARLY EXAMINATION (2023-24)

SUBJECT :PHYSICS (SET-2) CLASS : XII

	MARKING SCHEME					
Q. NO.	VALUE POINTS	MARKS ALLOTTED	PAGE NO. OF NCERT TEXT BOOK (OLD BOOK)			
	SECTION-A		,			
1	(c)	1	248			
2	(d)	1	47			
3	(c)	1	74			
4	(b)	1	98			
5	(a)	1	110			
6	(b)	1	98			
7	(d)	1	135			
8	(a)	1	192			
9	(b)	1	230			
10	(d)	1	212			
11	(c)	1	17			
12	(d)	1	282			
13	(a)	1	277			
14	(c)	1	104			
15	(b)	1	138			
16	(a)	1	222			
4=	SECTION-B					
17	The uniform charge –Q will be induced on inner surface of the shell	1				
	and +Q will be induced on outer surface. This is follows from conservation of					
	charge and no static charges reside in the interior of a metal in electrical					
	equilibrium.					
	Using Gauss's law the field at P <sub>1</sub> :	1	39			
	$E.4\pi r_1^2 = Q/\epsilon_0$					
	Where Qen= $+Q$ , charge inside Gaussian surface of radius $r_1$ .					
	Thus, $E=Q/4\pi\epsilon_0 r_1^2$					

18.	$\frac{q_1}{4\pi \in_0 r} = -\frac{q_2}{4\pi \in_0 (d-r)}$	0.5	87
	$\frac{q_1}{r} = \frac{-q_2}{d-r}$		
	$\frac{5 \times 10^{-8}}{r} = -\frac{\left(-3 \times 10^{-8}\right)}{\left(0.16 - r\right)}$		
	r = (0.16-r)		
	$\frac{0.16}{r} - 1 = \frac{3}{5}$		
		1	
	$\frac{0.16}{r} = \frac{8}{5}$	0.5	
	$\therefore r = 0.1 \mathrm{m} = 10 \mathrm{cm}$ OR		55
	(a) $V = \frac{1}{4\pi\epsilon_0} \frac{Q}{r} = 9 \times 10^9 \text{ Nm}^2 \text{ C}^{-2} \times \frac{4 \times 10^{-7} \text{ C}}{0.09 \text{ m}}$		33
	$= 4 \times 10^4  \text{V}$	1	
	(b) $W = qV = 2 \times 10^{-9} \text{C} \times 4 \times 10^{4} \text{V}$ = $8 \times 10^{-5} \text{J}$ No, work done will be path independent. Any arbitrary infinitesimal	0.5	
	path can be resolved into two perpendicular displacements: One along r and another perpendicular to r. The work done corresponding to	0.5	
	the later will be zero.	0.5	
19	The current in the circuit		128
	$I = \frac{E_1 - E_2}{R_{\text{ext}} + r} = \frac{120 - 8}{15.5 + 0.5}$		
	•	0.5	
	or $I = \frac{112}{16} = 7 \text{ A}$	0.5	
	Terminal voltage of the battery during charging : $V = E + lr = 8 + 7(0.5) = 11.5 \text{ V}$	0.5	
	A series resistance is joined in the charging circuit to limit the		
20	excessive current so that charging is slow and permanent. $mV^2$	0.5	138
	$\frac{dr}{r} = qVB$	0.5	
	$\Rightarrow r = \frac{mV}{qB}$		
		0.5	
	$v = \frac{V}{2\pi r}$		
	VqB	0.5	
	$v = \frac{1}{2\pi mV}$		
	$v = \frac{qB}{2\pi m}$	0.5	
	$V = \frac{1}{2\pi m}$	5.5	

Physics XII (Set-2)

PAGE-5

21.	(a) The bulb B lights because an emf is induced in coil Q due to change	1	206
	in magnetic flux crossing through it.		
	(b) Bulb gets dimmer if the coil Q is moved towards left because of	1	
	mutual induction, and hence induced emf in coil Q decreases with		
	separation between the coils.		
22	SECTION-C		21
22	(a)		31
	*************************************		
	- B 711-9L		
	2 <i>i</i> _ <del>0</del> = <del></del>	0.5	
	<del> </del>		
	⇒ <del>≠ •</del> • • • • • • • • • • • • • • • • • •		
	$\vec{F}_2 = -q\vec{E} \stackrel{F_A \setminus \theta}{\longleftarrow q} \cdots \cdots \cdots \cdots \cdots$		
	Net force on electric dipole in uniform electric field is		
	$F = F_1 - F_2 = qE - qE = 0$ . Thus there is no translational motion.	1	
	(b) Torque on the dipole		
	$\tau = F (2l \sin \theta) = qE 2l \sin \theta$		
	$\vec{\tau} = \vec{p} \times \vec{E}$		
	$\tau = p \times E$	1	
	The direction of torque is perpendicularly into the plane of paper	0.5	
	The direction of torque is perpendicularly into the plane of paper.	0.5	
23	(a) $Q = n q$	0.5	54
	(b)		
	4 - 3 4 3 - 1/3		
	$\frac{4}{3}\pi R^3 = n\frac{4}{3}\pi r^3  \Rightarrow  R = n^{1/3}r$	0.5	
	0		
	If potential of a small drop, $V = \frac{Q}{C}$ ;		
	nO		
İ	then potential of a big drop, $V' = \frac{nQ}{n^{1/3}C} = n^{2/3}V$	1	
	n C		
İ	(c) Capacity of each droplet, $C = 4\pi\epsilon_0 r$		
	Capacity of each dropiet, $C' = 4\pi\epsilon_0 R = 4\pi\epsilon_0 n^{1/3} r = n^{1/3} C$	1	
	Capacity of a big drop, $C = 4\pi\epsilon_0 h = 4\pi\epsilon_0 n + n + n + C$		
	OD		
	OR		
	(a) $V = \frac{KQ}{r}$		
	7 77		
	$Q = \frac{V}{K\left(\frac{1}{r}\right)}$	0.5	
	$\frac{Q_1}{Q_2} = \frac{\tan \theta_1}{\tan \theta_2} = \frac{\tan 60^0}{\tan 30^0} = 3:1$	1	
	$\frac{1}{Q_2} = \frac{1}{\tan \theta_2} = \frac{1}{\tan 30^0} = 3:1$	1	
		0.5	

	(b) $\frac{Q_1}{4\pi\epsilon_0 R_1} = \frac{Q_2}{4\pi\epsilon_0 R_2}$ $\frac{Q_1}{Q_2} = \frac{R_1}{R_2}$ $\frac{\sigma_1}{\sigma_2} = \frac{Q_1}{Q_2} \left(\frac{R_1}{R_2}\right)^2 = \frac{R_2}{R_1} \implies \frac{\sigma_2}{\sigma_1} = \frac{R_1}{R_2}$	1	
24	(a) Statement of the laws	1	116
	(b) $ \begin{array}{ccccccccccccccccccccccccccccccccccc$	0.5	
	For closed loop $ABCC'EA$ applying Kirchhoff's second rule. $-IR - \frac{I}{2}R - IR + \varepsilon = 0 \implies \varepsilon = \frac{5}{2}IR$ The equivalent resistance of the network is $R_{eq}, \text{ i.e. } R_{eq} = \frac{\varepsilon}{3I} = \frac{5}{6}R$ For $R = 1 \Omega$ , $R_{eq} = \frac{5}{6}\Omega$	0.5	
	14 0	0.5	
	OR		
	(a)		
	We know $V = \varepsilon_1 - I_1 r_1$ So, $I_1 = \frac{\varepsilon_1 - V}{r_1}$ Similarly, $I_2 = \frac{\varepsilon_2 - V}{r_2}$ Now, $I = I_1 + I_2$ $\therefore I = \left(\frac{\varepsilon_1 - V}{r_1}\right) + \left(\frac{\varepsilon_2 - V}{r_2}\right) \Rightarrow I = \left(\frac{\varepsilon_1}{r_1} + \frac{\varepsilon_2}{r_2}\right) - V\left(\frac{1}{r_1} + \frac{1}{r_2}\right) \dots (a)$	1	
	$I = \left(\frac{\varepsilon_1 r_2 + \varepsilon_2 r_1}{r_1 \cdot r_2}\right) - V\left(\frac{r_1 + r_2}{r_1 \cdot r_2}\right) \Rightarrow V = \left(\frac{\varepsilon_1 r_2 + \varepsilon_2 r_1}{r_1 + r_2}\right) - I\left(\frac{r_1 r_2}{r_1 + r_2}\right) \dots (b)$	0.5	114
	The expression for the equivalent emf of the combination $\varepsilon_1 r_2 + \varepsilon_2 r_1$	0.5	
	$\varepsilon_{eq} = \frac{1}{r_1 + r_2}$ (b) Expression for the equivalent resistance of the combination $r_1 r_2$	0.5	
	$r_{eq} = \frac{12}{r_1 + r_2}$	0.5	

25	$ \stackrel{\scriptstyle \sim}{\stackrel{\sim}{i}} \stackrel{\sim}{\stackrel{\sim}{i}} \stackrel{\vee}{\stackrel{\vee}{\longrightarrow}} \stackrel{\vee}{\stackrel{\vee}{\longrightarrow}} \stackrel{\vee}{\stackrel{\vee}{\longrightarrow}} \stackrel{\vee}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\vee}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow} \stackrel{\longrightarrow}{\longrightarrow$	0.5	140
	/I		
	For the charged particle to more undeflected		
	Net force $\overline{F} = \overline{F_E} + \overline{F_m} = 0$	0.5	
	$\frac{\vec{F}_E}{F_E} = -F_m \tag{1}$ $\frac{\vec{F}_E}{F_E} \to \text{electric force},  \overline{F_m} \to \text{magnetic force}$		
	$F_E \to \text{electric force}, F_m \to \text{magnetic force}$		
	$ \overline{F_E}  =  \overline{F_m} $		
	$qE = Bqv \sin 90^{\circ} = Bqv$		
	$E = VB \tag{3}$		
	$\mathbf{B} = \frac{\mathbf{MoI}}{2\pi \mathbf{r}} \tag{4}$		
	Using (4) and (3)		
	$E = \frac{VMoI}{2\pi r} $ (5)	1	
	Magnetic force $F_m$ is towards wire.	1	
	∴ Electric force and electric field should be away from the line.		
	<b>小</b> 屋		
	al se		
		1	
	<del> </del>		
26	(a) PQ <sub>1</sub> and PQ <sub>2</sub>	0.5 + 0.5	181
	(4) - (1) 11111 - (2)		
	(b) (i) PQ <sub>3</sub> , PQ <sub>6</sub> (stable); (ii) PQ <sub>5</sub> , PQ <sub>4</sub> (unstable)	0.5 + 0.5	
	$(c) PQ_6$	0.5	
	Reason:		
	$\mathbf{B}_{\mathrm{P}} = -\frac{\mu_0}{4\pi} \frac{\mathbf{m}_{\mathrm{P}}}{r^3}$ (on the normal bisector)		
		0.5	
	$\mathbf{B}_{\mathrm{p}} = \frac{\mu_0 2}{4\pi} \frac{\mathbf{m}_{\mathrm{p}}}{r^3} \qquad \text{(on the axis)}$		
27	T/1 1		266
21	(a)		266
	Given: $V_{\text{rms}} = 50 \text{ V}, v = \frac{50}{\pi} \text{ Hz}, R = 300 \Omega, C = 20 \times 10^{-6} \text{ F}, L = 1.0 \text{ H}$		
	n n	0.5	
	As we know $X_C = \frac{1}{2\pi vC} = \frac{1}{2\pi \times \frac{50}{\pi} \times 20 \times 10^{-6}} = 500 \ \Omega$	0.3	
	$2\pi \times \frac{50}{2} \times 20 \times 10^{-6}$		
	π		
	As we know $X_L = 2\pi v L = 2\pi \times \frac{50}{\pi} \times 1 = 100 \Omega$	0.5	
	$Z = \sqrt{R^2 + (X_C - X_L)^2} = \sqrt{90000 + (500 - 100)^2}$		
	$Z = \sqrt{K^2 + (X_C - X_L)^2} = \sqrt{90000 + (500 - 100)^2}$		
	$Z = \sqrt{90000 + 160000} = \sqrt{250000} = 500 \Omega$	0.5	
	,	0.5	
	1	1	i l

		1	
	(h)		
	(b)		
	$I_{\rm rms} = \frac{50}{5 \times 10^2} = 0.1 \text{ A}$	0.5	
	5×10 <sup>2</sup>	0.0	
	$\begin{pmatrix} c \\ R \end{pmatrix} = \begin{pmatrix} R \\ R \end{pmatrix} = \begin{pmatrix} R \\ R \end{pmatrix}$		
	Power factor $\cos \emptyset = \frac{R}{Z} = \frac{3}{5} = 0.6$	1	
20			207
28	$E_{y} = E_{0}\cos(\omega t - hx) \text{ N/C}$		287
	$E_0 = 4 \times 10^5 \text{ N/C}, \ \omega = 3.14 \times 10^8 \text{ rad s}^{-1}, \ k = 1.57 \text{ rad.m}^{-1}$		
	(a)		
	$v = \frac{\omega}{k} = \frac{3.14 \times 10^8}{1.57}$ m/s = 2 × 10 <sup>8</sup> m/s	1	
	$v = \frac{1.57}{k} = \frac{1.57}{1.57} \text{ m/s} = 2 \times 10^{6} \text{ m/s}$		
	(b)		
	$\mu = \frac{c}{v} = \frac{3 \times 10^8}{2 \times 10^8} = 1.5$	1	
	(C) F <sub>2</sub> F <sub>3</sub> A > 10 <sup>5</sup>	1	
	$\frac{E_0}{B_0} = c \Rightarrow B_0 = \frac{E_0}{c} = \frac{4 \times 10^5}{3 \times 10^8} \text{T} = 1.33 \times 10^{-3} \text{ T}$	1	
	SECTION-D		
29	(i) (c)	1	73,81
2)	(ii) (d)	1	75,01
	(iii) (b)	1	
	(iv) (a)	1	
	OR		
	(iv) (b)	1	
30	(i) (c)	1	222,224
	(ii) (b)	1	
	(iii) (a) (iv) (b)	1	
	OR		
	(iv) (d)	1	
	SECTION-E		
31	C R		245
		0.5	
		0.5	
	(a)		
	Q V <sub>mR</sub>		
	V <sub>mL</sub> V <sub>m</sub>		
	oot		
	0		
	V <sub>mC</sub> – V <sub>mL</sub>		
	V <sub>m</sub> c	1	
		1	

## On applying Pythagoras theorem, we get $V_{\rm m}^2 = V_{\rm Rm}^2 + (V_{\rm Cm} - V_{\rm Lm})^2$ Here $V_{\mathit{Rm}} = I_{\mathit{m}}R, \; V_{\mathit{Cm}} = I_{\mathit{m}}X_{\mathit{C}}, V_{\mathit{Lm}} = I_{\mathit{m}}X_{\mathit{L}}$ 1 $V_{\rm m} = I_{\rm m} \sqrt{R^2 + (X_{\rm C} - X_{\rm L})^2}$ $V_{\rm m} = I_{\rm m} Z$ $Z = \sqrt{R^2 + (X_C - X_I)^2}$ where, Z is called the impedance of the circuit. (b) 0.5 $\phi = \tan^{-1} \left( \frac{V_{Cm} - V_{Lm}}{V_{Rm}} \right)$ 0.5 0.5 $I = I_m \sin (\omega t + \phi)$ (c) 1 N. B.- Award marks for $X_L > X_c$ OR 259 (a) Soft iron-core 0.5

Principle – Based on the principle of mutual induction  (b) Assumptions- (i) the primary resistance and current are small; (ii) the same flux links both the primary and the secondary as very little flux escapes from the core, and (iii) the secondary current is small.  Theory- $\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t} \qquad \varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ 0.5  If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $i_p v_p = i_s v_s$ (c) The large scale transmission and distribution of electrical energy			
(i) the primary resistance and current are small; (ii) the same flux links both the primary and the secondary as very little flux escapes from the core, and (iii) the secondary current is small.    Theory- $\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t} \qquad \varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ 0.5  If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $i_p v_p = i_s v_s$ $i_p v_p = i_s v_s$ 0.5		0.5	
(ii) the same flux links both the primary and the secondary as very little flux escapes from the core, and (iii) the secondary current is small.    Theory- $\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t} \qquad \varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ 0.5  If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$ 0.5			
flux escapes from the core, and (iii) the secondary current is small.    Theory- $\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t} \qquad \varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ 0.5  1. The transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output, and since $p = i v$ , the power input is equal to the power output.	(i) the primary resistance and current are small;		
(iii) the secondary current is small. Theory- $\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t} \qquad \varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ 0.5 $\frac{v_s}{v_p} = \frac{N_s}{N_p}$ If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $\frac{i_p}{v_p} = i_s v_s$ 0.5	(ii) the same flux links both the primary and the secondary as very little		
Theory- $\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t} \qquad \varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ 0.5  If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$	flux escapes from the core, and		
$\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t} \qquad \varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $v_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ 0.5  If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$ 0.5	(iii) the secondary current is small.	1	
But $\varepsilon_p = V_p$ . If this were not so, the primary current would be infinite since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{d\phi}{dt}$ $v_p = -N_p \frac{d\phi}{dt}$ 0.5  If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$ 0.5	Theory-		
since the primary has zero resistance(as assumed). If the secondary is an open circuit or the current taken from it is small, then to a good approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{d\phi}{dt}$ $v_p = -N_p \frac{d\phi}{dt}$ 0.5  If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = iv$ , $i_p v_p = i_s v_s$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$ 0.5	$\varepsilon_p = -N_p \frac{\mathrm{d}\phi}{\mathrm{d}t}$ $\varepsilon_s = -N_s \frac{\mathrm{d}\phi}{\mathrm{d}t}$		
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approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary. $v_s = -N_s \frac{d\phi}{dt}$ $v_p = -N_p \frac{d\phi}{dt}$ $v_p = \frac{N_s}{N_p}$ If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $i_p v_p = i_s v_s$ $0.5$	since the primary has zero resistance(as assumed). If the secondary is		
$v_{s} = -N_{s} \frac{d\phi}{dt}$ $v_{p} = -N_{p} \frac{d\phi}{dt}$ $0.5$ $\frac{v_{s}}{v_{p}} = \frac{N_{s}}{N_{p}}$ If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_{p}v_{p} = i_{s}v_{s}$ $\frac{i_{p}}{i_{s}} = \frac{v_{s}}{v_{p}} = \frac{N_{s}}{N_{p}}$ $0.5$	an open circuit or the current taken from it is small, then to a good		
$v_p = -N_p \frac{d\phi}{dt}$ $\frac{v_s}{v_p} = \frac{N_s}{N_p}$ If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$ 0.5	approximation $\varepsilon_s = V_s$ where $V_s$ is the voltage across the secondary.		
If the transformer is assumed to be 100% efficient (no energy losses), the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $i_p v_p = i_s v_s$ $0.5$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$	$v_s = -N_s \frac{d\phi}{dt}$		
the power input is equal to the power output, and since $p = i v$ , $i_p v_p = i_s v_s$ $\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$ 0.5	$v_p = -N_p \frac{d\phi}{dt}$	0.5	
the power input is equal to the power output, and since $p = i v$ , $ \frac{i_p}{i_s} v_p = i_s v_s $ $ \frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p} $ 0.5	$\frac{v_s}{v_p} = \frac{N_s}{N_p}$		
$ \frac{\mathbf{i}_p \mathbf{v}_p = \mathbf{i}_s \mathbf{v}_s}{\mathbf{i}_s} = \frac{\mathbf{v}_s}{\mathbf{v}_p} = \frac{N_s}{N_p} $ 0.5	If the transformer is assumed to be 100% efficient (no energy losses),	0.5	
$\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p} \tag{0.5}$	the power input is equal to the power output, and since $p = i v$ ,		
$\frac{v_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$	$i_p v_p = i_s v_s$		
0.5	$\frac{i_p}{i_s} = \frac{v_s}{v_p} = \frac{N_s}{N_p}$	0.5	
		0.5	
over long distances is done with the use of transformers. The voltage	over long distances is done with the use of transformers. The voltage		
output of the generator is stepped-up (so that current is reduced and		1	
consequently, the $I^2R$ loss is cut down).			

32.	(a) Gauss's Law states that the net outward flux through any closed		39,35
	surface is equal to $\frac{1}{\epsilon_0}$ times the charge enclosed by the closed surface.	0.5	
	(i) When the point <i>P</i> is inside the shell.		
	In this case, the Gaussian surface lies inside the spherical shell and		
	hence no charge is enclosed by it.	0.5	
	$\oint \vec{E} \cdot \vec{ds} = \frac{1}{\varepsilon_0} \times 0 = 0$		
	or $E = 0$ , i.e. there is no electric field inside a charged spherical shell.		
	(ii) When the point <i>P</i> lies outside the shell		
	At every point of this shell, the $\vec{E}$ and $\vec{ds}$ are directed outwards in the		
	same direction, i.e. $\theta = 0$ .	0.5	
		0.5	
	$Q = \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{\vec{Q}} + \frac{\vec{R}}{$		
	$\therefore \oint \vec{E}  d\vec{s} = \oint E  ds = E \oint ds = E \times 4\pi r_2^2 \qquad(i)$ Also, by Gauss's law		
	$ \oint \vec{E}  d\vec{s} = \frac{1}{\varepsilon_0} Q \qquad(\vec{n}) $		
	From (i) and (ii), we get		
	$E \times 4\pi r^2 = \frac{1}{\varepsilon_0} Q \implies E = \frac{1}{4\pi\varepsilon_0} \frac{Q}{r^2} \qquad [\because r = r_2]$		
		1.5	
	(b)		
	$q = \epsilon_0 \phi = \epsilon_0 (\phi_R + \phi_L)$		28,16
	$=\epsilon_0(4a^3-2a^3)=2\epsilon_0a^3$	1+1	
	OR		
	(a)		
	$E_{+q} \sin \theta$ $E_{+q} \cos \theta$ $E_{-q} \cos \theta$ $E_{-q} \sin \theta$ $E_{-q} \cos \theta$	1	
	!2a <u>.</u>		

	<u> </u>	1	
	$\vec{E} = -(E_{+q} + E_{-q}) \cos \theta \hat{p}$		
	$\vec{E} = -\frac{2qa}{4\pi \varepsilon_0 (x^2 + a^2)^{3/2}} \hat{p}$		
	$\vec{E} = -\frac{\vec{p}}{4\pi \varepsilon_0 (x^2 + a^2)^{3/2}}$	1.5	
	For $x \gg a$	0.5	
	$\overrightarrow{E} = -\frac{1}{4\pi\epsilon_0} \frac{\overrightarrow{P}}{x^3}$		
	(b) $\vec{F} = k \frac{q_1 q_2}{r^2} \hat{r}$		
	$r = \sqrt{2}a$ $\hat{\imath} + \hat{\jmath}$		
	$\hat{r} = \frac{\hat{\imath} + \hat{\jmath}}{\sqrt{2}}$	2	
	$\vec{F} = k \ q \cdot \frac{2q}{(\sqrt{2}a)^2} \left(\frac{\hat{i}+\hat{j}}{\sqrt{2}}\right) = \frac{kq^2}{\sqrt{2}a^2} (\hat{i}+\hat{j})N$		
22			1.45
33	(a)		145
	dB cos $\phi$ $\phi$ $\phi$ $\phi$ $\phi$ $\phi$ $\phi$ $\phi$ $\phi$ $\phi$	1	
	$ \overrightarrow{dB}  = \frac{\mu_0}{4\pi} \frac{Idl \sin 90^\circ}{S^2}$		
	$dB = \frac{\mu_0}{4\pi} \frac{Idl}{S^2} = \frac{\mu_0}{4\pi} \frac{Idl}{(r^2 + x^2)} (\because S = \sqrt{r^2 + x^2})$ The direction of $\overline{dB}$ is perpendicular to the plane		
	containing $\vec{S}$ and $\vec{dl}$ . We resolve $\vec{dB}$ into rectangular components $dB$ cos $\phi$ and $dB$ sin $\phi$ .		

Thus, total magnetic field is given by $B = \int dB \sin \phi = \int \frac{\mu_0 I dl \sin \phi}{4\pi (r^2 + x^2)}$ $B = \frac{\mu_0 I}{4\pi (r^2 + x^2)} \frac{r}{(x^2 + r^2)^{1/2}} \cdot 2\pi r$ $= \frac{\mu_0 I r^2}{2 (r^2 + x^2)^{3/2}}$	2	
(b)Since the total length of the wire used remains the same,		
$N \times \pi d = N' \times \pi (2d)$	1	
N'=N / 2		
Hence the ratio of the magnetic moments=M/M'		
=INA/IN'A'		
$=NA/N'A'=Nd^2/N'd'^2=2$ $M'/M=1/2$	1	
OR		
(a) $ \begin{array}{cccc} X' & & & Y' \\ \downarrow i_1 & & & \downarrow i_2 \end{array} $ $ \begin{array}{ccccc} F_X & F_Y & \otimes \\ & & & & & \\ X & & & & & \\ X & & & & & \\ X & & & & & \\ \end{array} $	0.5	154
The magnitude of magnetic field at each point on Y' due to current $i_1$ in XX' is given by $B_1 = \frac{\mu_0}{2\pi} \cdot \frac{i_1}{R}$		
$F_Y = i_2 B_1 l = i_2 \frac{\mu_0}{2\pi} \cdot \frac{i_1}{R} \cdot l$ Force per unit length of YY' is given by $\frac{F_Y}{l} = \frac{\mu_0}{2\pi} \cdot \frac{i_1 i_2}{R}$	0.5	
Similarly		
$\frac{F_X}{l} = \frac{\mu_0}{2\pi} \cdot \frac{i_1 i_2}{R}$	0.5	
The force is attractive in nature.	0.3	

The <i>ampere</i> is the value of that steady current which, when maintained in each of the two very long, straight, parallel conductors of negligible cross-section, and placed one metre apart in vacuum, would produce on each of these conductors a force equal to $2 \times 10^{-7}$ newtons per metre of length.	1
(b) <i>F</i>	
$C \xrightarrow{I_2 = 5 \text{ A}} D \xrightarrow{\uparrow} W = mg \qquad 1 \text{ mm} = r$	0.5
AB ♥	
$F = \frac{\mu_0}{4\pi} \cdot \frac{2I_1I_2}{r} = mg$	
$m = \frac{\mu_0}{4\pi} \cdot \frac{2I_1I_2}{rg}$	0.5
$m = \frac{10^{-7} \times 12 \times 5 \times 2}{1 \times 10^{-3} \times 10}$	
$m = 12 \times 10^{-4} \text{ kg-m}^{-1}$ The direction of current in wire <i>CD</i> will be opposite to the	0.5
direction of current in wire $AB$ .	
	0.5